

**1011 – I2 - 1**

Ako su

$$\Phi = r \sin(\pi\varphi + \vartheta); \quad \vec{F} = r^2 \sin \vartheta \hat{r} + r \cos \varphi \hat{\vartheta} + \cos \vartheta \hat{\varphi}; \quad M = \log_2 \sin x^{y+z}; \quad \vec{E} = \frac{\rho}{z} \hat{\rho}$$

gdje su  $(r, \vartheta, \varphi)$  Kartezijeve koordinate,  $(r, \vartheta, \varphi)$  sferne koordinate, a  $(\rho, \varphi, z)$  cilindrične, odredite u pripadnom koordinatnom sustavu

- (a)  $\nabla\Phi$ ;                      (b)  $\nabla\vec{F}$ ;                      (c)  $\nabla \times \vec{E}$ ;                      (d)  $\text{rot}(\nabla M)$ .

U ortogonalnim koordinatnim sustavima dani su opći izrazi za gradijent, divergenciju, rotaciju i laplasijan

$$\nabla\Phi = \sum_{i=1}^3 \frac{1}{h_i} \cdot \frac{\partial\Phi}{\partial q_i} \hat{q}_i$$

$$\nabla\vec{F} = \frac{1}{h_1 h_2 h_3} \sum_{i(j,k)} \frac{\partial}{\partial q_i} (h_j h_k F_i)$$

$$\nabla \times \vec{F} = \frac{1}{h_1 h_2 h_3} \begin{vmatrix} h_1 \hat{q}_1 & h_2 \hat{q}_2 & h_3 \hat{q}_3 \\ \frac{\partial}{\partial q_1} & \frac{\partial}{\partial q_2} & \frac{\partial}{\partial q_3} \\ h_1 F_1 & h_2 F_2 & h_3 F_3 \end{vmatrix}$$

$$\Delta = \frac{1}{h_1 h_2 h_3} \sum_{i(j,k)} \frac{\partial}{\partial q_i} \left( \frac{h_j h_k}{h_i} \cdot \frac{\partial}{\partial q_i} \right)$$

gdje su  $h_i$  Lamoevi koeficijenti koji iznose za

Kartezijev koordinatni sustav	cilindrični koordinatni sustav	sferni koordinatni sustav
$h_1 = 1$	$h_1 = 1$	$h_1 = 1$
$h_2 = 1$	$h_2 = r$	$h_2 = \rho$
$h_3 = 1$	$h_3 = r \sin \vartheta$	$h_3 = 1$

**Gradijent u sfernom**

$$\nabla\Phi = \frac{1}{h_1} \cdot \frac{\partial\Phi}{\partial q_1} \hat{q}_1 + \frac{1}{h_2} \cdot \frac{\partial\Phi}{\partial q_2} \hat{q}_2 + \frac{1}{h_3} \cdot \frac{\partial\Phi}{\partial q_3} \hat{q}_3$$

$$\nabla\Phi = \frac{1}{r} \cdot \frac{\partial\Phi}{\partial r} \hat{r} + \frac{1}{r} \cdot \frac{\partial\Phi}{\partial \vartheta} \hat{\vartheta} + \frac{1}{r \sin \vartheta} \cdot \frac{\partial\Phi}{\partial \varphi} \hat{\varphi}$$

$$\nabla\Phi = \frac{1}{r} \cdot \sin(\pi\varphi + \vartheta) \hat{r} + \frac{1}{r} \cdot r \cos(\pi\varphi + \vartheta) \hat{\vartheta} + \frac{1}{r \sin \vartheta} \cdot r \pi \cos(\pi\varphi + \vartheta) \hat{\varphi}$$

$$\nabla\Phi = \sin(\pi\varphi + \vartheta) \hat{r} + \cos(\pi\varphi + \vartheta) \hat{\vartheta} + \frac{\pi}{\sin \vartheta} \cos(\pi\varphi + \vartheta) \hat{\varphi}$$

**Divergencija u sfernom**

$$\nabla\vec{F} = \frac{1}{h_1 h_2 h_3} \left\{ \frac{\partial}{\partial q_1} (h_2 h_3 \cdot F_1) + \frac{\partial}{\partial q_2} (h_3 h_1 \cdot F_2) + \frac{\partial}{\partial q_3} (h_1 h_2 \cdot F_3) \right\}$$

$$\nabla\vec{F} = \frac{1}{r^2 \sin \vartheta} \left\{ \frac{\partial}{\partial r} (r^2 \sin \vartheta \cdot r^2 \sin \vartheta) + \frac{\partial}{\partial \vartheta} (r \sin \vartheta \cdot r \cos \varphi) + \frac{\partial}{\partial \varphi} (r \cdot \cos \vartheta) \right\}$$

$$\nabla\vec{F} = \frac{1}{r^2 \sin \vartheta} (4r^3 \sin^2 \vartheta + r^2 \cos \vartheta \cdot \cos \varphi + 0)$$

$$\nabla\vec{F} = 4r \sin \vartheta + \text{ctg} \vartheta \cdot \cos \varphi$$

## Rotacija u cilindričnom

$$\nabla \times \vec{E} = \frac{1}{h_1 h_2 h_3} \begin{vmatrix} h_1 \hat{q}_1 & h_2 \hat{q}_2 & h_3 \hat{q}_3 \\ \frac{\partial}{\partial q_1} & \frac{\partial}{\partial q_2} & \frac{\partial}{\partial q_3} \\ h_1 F_1 & h_2 F_2 & h_3 F_3 \end{vmatrix}$$

$$\nabla \times \vec{E} = \frac{1}{\rho} \begin{vmatrix} 1 \cdot \hat{\rho} & \rho \cdot \hat{\varphi} & 1 \cdot \hat{z} \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \varphi} & \frac{\partial}{\partial z} \\ 1 \cdot \frac{\rho}{z} & \rho \cdot 0 & 1 \cdot 0 \end{vmatrix} = \frac{1}{\rho} \begin{vmatrix} \hat{\rho} & \rho \hat{\varphi} & \hat{z} \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \varphi} & \frac{\partial}{\partial z} \\ \frac{\rho}{z} & 0 & 0 \end{vmatrix}$$

$$\nabla \times \vec{E} = \frac{\hat{\rho}}{\rho} \left[ \frac{\partial}{\partial \varphi} (0) - \frac{\partial}{\partial z} (0) \right] + \hat{\varphi} \left[ \frac{\partial}{\partial z} \left( \frac{\rho}{z} \right) - \frac{\partial}{\partial \rho} (0) \right] + \frac{\hat{z}}{\rho} \left[ \frac{\partial}{\partial \rho} (0) - \frac{\partial}{\partial \varphi} \left( \frac{\rho}{z} \right) \right]$$

$$\nabla \times \vec{E} = \frac{\hat{\rho}}{\rho} [0 - 0] + \hat{\varphi} \left[ -\frac{\rho}{z^2} - 0 \right] + \frac{\hat{z}}{\rho} [0 - 0]$$

$$\nabla \times \vec{E} = -\frac{\rho}{z^2} \hat{\varphi}$$

Identitet  $\nabla \times (\nabla \Phi) = 0$ 

$$\text{rot}(\nabla M) = 0$$

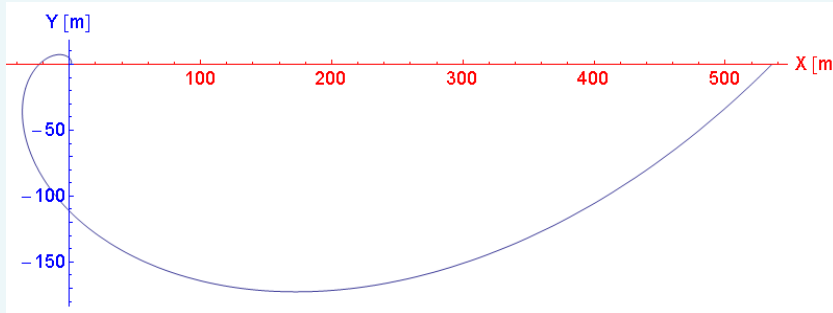
**1011 – I2 - 2**

Odredite rad sile (koordinate su izražene u metrima)

$$\vec{F} = \frac{x\hat{i} + y\hat{j}}{(x^2 + y^2)^{\frac{3}{2}}} [\text{Nm}^2]$$

na putu od točke (1,0)m do točke (e<sup>2π</sup>,0)m po krivulji

$$\vec{r}(t) = (e^t \cos t)\hat{i} + (e^t \sin t)\hat{j}$$



Rad sile duž krivulje C iznosi

$$W = \int_C \vec{F} \cdot d\vec{r} = \int_C \vec{F} \cdot (dx\hat{i} + dy\hat{j})$$

**Parametrizacija**

Kako je putanja

$$\vec{r} = x\hat{i} + y\hat{j}$$

već zadana parametrizirana

$$\vec{r}(t) = (e^t \cos t)\hat{i} + (e^t \sin t)\hat{j}$$

zaključujemo

$$x = e^t \cos t \Rightarrow dx = (e^t \cos t - e^t \sin t)dt$$

$$y = e^t \sin t \Rightarrow dy = (e^t \sin t + e^t \cos t)dt$$

Prema tome sila je

$$\vec{F} = \frac{e^t \cos t \hat{i} + e^t \sin t \hat{j}}{((e^t \cos t)^2 + (e^t \sin t)^2)^{\frac{3}{2}}} = \frac{e^t \cos t \hat{i} + e^t \sin t \hat{j}}{e^{3t}} [\text{N}]$$

**Granice integracije**

Kako ćemo integrirati po t, potrebno je odrediti i njegove granične vrijednosti:

Početna točka A(1,0)

$$(1) \quad x = e^t \cos t = 1 \xrightarrow{(2)/(1)} \text{tg } t = 0 \Rightarrow t = k\pi$$

$$(2) \quad y = e^t \sin t = 0 \xrightarrow{} k \in \mathbb{Z}$$

$$(1) \Rightarrow t = \ln(1/\cos t) \xrightarrow{\text{Arg}(\ln) > 0} t = \ln\left(\frac{1}{1}\right) = 0$$

$$(R) \Rightarrow \cos(k\pi) = \pm 1 \xrightarrow{} t = \ln(e^{2\pi})$$

$$t_A = 0$$

Krajnja točka B(e<sup>2π</sup>,0)

$$(1) \quad x = e^t \cos t = e^{2\pi} \xrightarrow{(2)/(1)} \text{tg } t = 0 \Rightarrow t = k\pi$$

$$(2) \quad y = e^t \sin t = 0 \xrightarrow{} k \in \mathbb{Z}$$

$$(1) \Rightarrow t = \ln(e^{2\pi}/\cos t) \xrightarrow{\text{Arg}(\ln) > 0} t = \ln(e^{2\pi})$$

$$(R) \Rightarrow \cos(k\pi) = \pm 1 \xrightarrow{} t = \ln(e^{2\pi})$$

$$t_B = 2\pi$$

Prema tome rad iznosi

$$W = \int_C \vec{F} \cdot (dx\hat{i} + dy\hat{j}) = \int_{t_A}^{t_B} \left[ \frac{e^t \cos t \hat{i} + e^t \sin t \hat{j}}{e^{3t}} \right] \cdot [(e^t \cos t - e^t \sin t)dt\hat{i} + (e^t \sin t + e^t \cos t)dt\hat{j}]$$

$$W = \int_0^{2\pi} \frac{e^t \cos t (e^t \cos t - e^t \sin t) + e^t \sin t (e^t \sin t + e^t \cos t)}{e^{3t}} dt$$

$$W = \int_0^{2\pi} \frac{e^{2t} \cos^2 t - e^{2t} \sin t \cos t + e^{2t} \sin^2 t + e^{2t} \sin t \cos t}{e^{3t}} dt$$

$$W = \int_0^{2\pi} \frac{e^{2t} (\cos^2 t + \sin^2 t)}{e^{3t}} dt$$

$$W = \int_0^{2\pi} e^{-t} dt = - \int_0^{2\pi} e^{-t} d(-t)$$

$$W = -e^{-t} \Big|_{\varphi=0}^{\varphi=2\pi} = -e^{-2\pi} + e^{-0}$$

$$W = (1 - e^{-2\pi})$$

$$W = \frac{e^{2\pi} - 1}{e^{2\pi}} \text{ J}$$

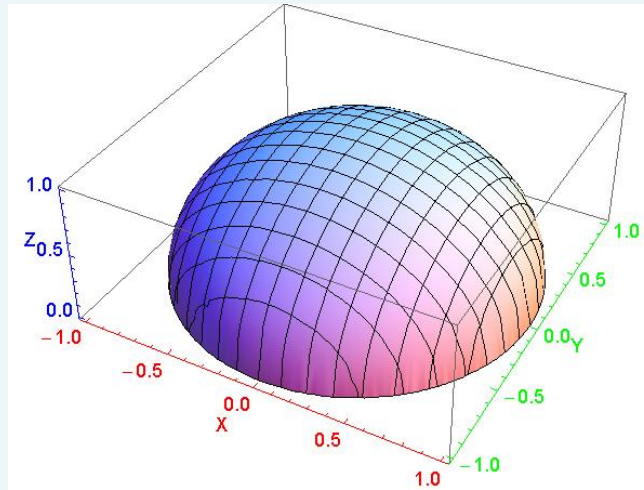
**1011 - I2 - 3**

Odredite masu tijela u obliku polovice kugle (koordinate su izražene u metrima)

$$x^2 + y^2 + z^2 \leq 1 \text{ m}^2$$

iznad xy ravnine, ako ima promjenjivu gustoću

$$\rho = 7700 \text{ kgm}^{-3} + 160z \text{ kgm}^{-4}.$$



Masa tijela iznosi

$$M = \int_V \rho dV$$

**Granice integracije**

Integriramo po kugloj ( $x^2 + y^2 + z^2 \leq r^2$ ) polovici iznad xy ravnine ( $z \geq 0$ ) pa je najlakše integraciju vršiti u sfernom koordinatnom sustavu.

koordinate:	element volumena:	zadana kuglina polovica:
$x = r \sin \vartheta \cos \varphi$	$dV = r^2 \sin \vartheta dr d\vartheta d\varphi$	$0 \leq r \leq 1$
$y = r \sin \vartheta \sin \varphi$		$0 \leq \vartheta \leq \pi/2$
$z = r \cos \vartheta$		$0 \leq \varphi \leq 2\pi$

$$M = \int_V \rho dV = \iiint_V \rho r^2 \sin \vartheta dr d\vartheta d\varphi = \iiint_V (7700 + 160r \cos \vartheta) r^2 \sin \vartheta dr d\vartheta d\varphi = M_1 + M_2$$

$$M = 7700 \int_0^{\pi/2} d\vartheta \int_0^{2\pi} d\varphi \int_0^1 r^2 \sin \vartheta dr + 160 \int_0^{\pi/2} d\vartheta \int_0^{2\pi} d\varphi \int_0^1 r^3 \sin \vartheta \cos \vartheta dr = M_1 + M_2$$

$$M_1 = 7700 \int_0^{\pi/2} d\vartheta \int_0^{2\pi} d\varphi \int_0^1 r^2 \sin \vartheta dr = 7700 \int_0^{\pi/2} \sin \vartheta d\vartheta \int_0^{2\pi} d\varphi \left[ \frac{r^3}{3} \right]_{r=0}^{r=1} = \frac{7700}{3} \int_0^{\pi/2} \sin \vartheta d\vartheta [\varphi]_{\varphi=0}^{\varphi=2\pi}$$

$$M_1 = \frac{15400}{3} \pi \int_0^{\pi/2} \sin \vartheta d\vartheta = \frac{15400}{3} \pi [-\cos \vartheta]_{\vartheta=0}^{\vartheta=\pi/2} = \frac{15400}{3} \pi [-0 + 1] = \frac{15400}{3} \pi \text{ kg}$$

$$M_2 = 160 \int_0^{\frac{\pi}{2}} d\vartheta \int_0^{2\pi} d\varphi \int_0^1 r^3 \sin \vartheta \cos \vartheta dr = 160 \int_0^{\frac{\pi}{2}} \frac{\sin(2\vartheta)}{2} d\vartheta \cdot [\varphi]_{\varphi=0}^{\varphi=2\pi} \cdot \left[ \frac{r^4}{4} \right]_{r=0}^{r=1}$$

$$M_2 = 80 \int_0^{\frac{\pi}{2}} \sin(2\vartheta) d\vartheta \cdot [2\pi] \cdot \left[ \frac{1}{4} \right] = \frac{80\pi}{2} \int_0^{\frac{\pi}{2}} \sin(2\vartheta) \cdot \frac{d(2\vartheta)}{2} = \frac{80\pi}{2} \int_0^{\frac{\pi}{2}} \sin(2\vartheta) \cdot \frac{d(2\vartheta)}{2}$$

$$M_2 = -20\pi \cdot [\cos(2\vartheta)]_{\vartheta=0}^{\vartheta=\frac{\pi}{2}} = -20\pi \cdot [-1 - 1] = 40\pi \text{ kg}$$

$$M = M_1 + M_2 = \frac{15400}{3}\pi \text{ kg} + 40\pi \text{ kg} = \frac{15520}{3}\pi \text{ kg}$$

$$M = \frac{15520}{3}\pi \text{ kg}$$

**1011 - I2 - 4**

Od svih mogućih kvadara, definiranih nejednadžbama  $0 \leq x \leq a$ ,  $0 \leq y \leq b$ ,  $0 \leq z \leq 1$ , odredite onaj za koji je ukupni tok polja

$$\vec{F} = (-x^2 - 4xy)\hat{i} - 6yz\hat{j} + 12z\hat{k}$$

prema vani kroz svih 6 površina najveći. Koliko iznosi najveći tok?

Volumen kvadra  $V$  zatvoreno je područje u prostoru čiji je rub orjentabilna po dijelovima glatka ploha  $\vec{S}$ , koja ne presjeca samu sebe, a  $\vec{F} = (-x^2 - 4xy)\hat{i} - 6yz\hat{j} + 12z\hat{k}$  vektorsko polje klase  $C^1(V)$  pa možemo primijeniti **Gaussov teorem o divergenciji**

$$\oiint_S \vec{F} \cdot d\vec{S} = \iiint_V \nabla \vec{F} \cdot dV$$

Divergencija polja  $\nabla \vec{F}$

$$\nabla \vec{F} = \frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} + \frac{\partial F_z}{\partial z} = -2x - 4y - 6z + 12$$

Granice integracije

Kako su granične plohe ravnine, najjednostavnije je računati s Kartezijevim koordinatama  $(x, y, z)$ . Granice integracije zadane su definicijom kvadara

$$\begin{aligned} 0 &\leq x \leq a \\ 0 &\leq y \leq b \\ 0 &\leq z \leq 1 \end{aligned}$$

Sada imamo sve potrebne elemente za integriranje pa možemo izračunati ukupni tok polja

$$\begin{aligned} \oiint_S \vec{F} \cdot d\vec{S} &= \iiint_V \nabla \vec{F} \cdot dV = \int_0^a dx \int_0^b dy \int_0^1 (-2x - 4y - 6z + 12) \cdot dz = \\ &= \int_0^a dx \int_0^b dy (-2xz - 4yz - 3z^2 + 12z)|_{z=0}^{z=1} = \int_0^a dx \int_0^b dy (-2x - 4y - 3 + 12) = \\ &= \int_0^a dx (-2xy - 2y^2 + 9y)|_{y=0}^{y=b} = \int_0^a dx (-2xb - 2b^2 + 9b) = \\ &= (-x^2b - 2b^2x + 9bx)|_{x=0}^{x=a} = -a^2b - 2ab^2 + 9ab = f(a, b) \end{aligned}$$

Dakle, traženi je tok funkcija dviju varijabli (duljina stranica kvadra  $a, b$ ) pa ćemo kvadar za koji je tok maksimalan odrediti tražeći maksimum te funkcije.

NUŽNI UVJETI

Ekstreme funkcije  $f(x_1, \dots, x_n)$  ispitujemo u točkama  $x_0 = (x_{01}, \dots, x_{0n})$  u kojima nije definirana  $df$  i onima koje dobijemo rješavajući sustav

$$\left(\frac{\partial f}{\partial x_i}\right)_{x_0} = 0 \quad (\forall i = 1, \dots, n)$$

Nađemo sve parcijalne derivacije prvog reda i izjednačimo s nulom

$$\frac{\partial f}{\partial a} = -2ab - 2b^2 + 9b = 0 \quad \Rightarrow \quad -b(2b + 2a - 9) = 0 \quad (1)$$

$$\frac{\partial f}{\partial b} = -a^2 - 4ab + 9a = 0 \quad \Rightarrow \quad -a(a + 4b - 9) = 0 \quad (2)$$

Iz (2) i (1) imamo 4 mogućnosti iz kojih nalazimo 4 kandidata za točke ekstrema

$a = 0$	$a = 0$	$a + 4b - 9 = 0$	$a + 4b = 9$
$b = 0$	$2b + 2a - 9 = 0$	$b = 0$	$2a + 2b = 9$
$a = 0$	$a = 0$	$a = 9$	$a = 3$
$b = 0$	$b = 4.5$	$b = 0$	$b = 1.5$
$K_1(0, 0)$	$K_2(0, 4.5)$	$K_3(9, 0)$	$K_4(3, 1.5)$

**DOVOLJNI UVJETI**

Odredimo determinante za funkciju  $f(x_1, x_2, \dots, x_n)$ :

$$\Delta_r = \begin{vmatrix} a_{11} & \dots & a_{1r} \\ \vdots & \ddots & \vdots \\ a_{r1} & \dots & a_{rr} \end{vmatrix} ; \quad 1 \leq r \leq n ; \quad a_{ij} = \left( \frac{\partial^2 f}{\partial x_i \partial x_j} \right)_{x_0}$$

Funkcija  $f$  u točki  $x_0$ :

- ima MINIMUM, ako je  $(\Delta_r > 0) (\forall r)$
- ima MAKSIMUM, ako je  $\begin{cases} (\Delta_r > 0) (\forall r = 2k) \\ (\Delta_r < 0) (\forall r = 2k - 1) \end{cases}$
- NEMA EKSTREMA, ako je  $(\Delta_r \neq 0) \wedge \overline{(1)} \wedge \overline{(2)}$
- NEMA ODLUKE, ako  $(\exists \Delta_r = 0)$  pa su potrebna dodatna ispitivanja ( $df$ )

Kako bismo provjerili, radi li se o ekstremima, moramo odrediti druge parcijalne derivacije

$$\frac{\partial^2 f}{\partial a^2} = -2b \qquad \frac{\partial^2 f}{\partial a \partial b} = -2a - 4b + 9$$

$$\frac{\partial^2 f}{\partial b \partial a} = -2a - 4b + 9 \qquad \frac{\partial^2 f}{\partial b^2} = -4a$$

pa imamo

$$\Delta_1 = |-2b| = -2b \qquad \Delta_2 = \begin{vmatrix} -2b & -2a - 4b + 9 \\ -2a - 4b + 9 & -4a \end{vmatrix} = 8ab - (2a + 4b - 9)^2$$

koje u dobivenim točkama iznose

$\Delta_1(K_1) = 0$	$\Delta_1(K_2) = -9$	$\Delta_1(K_3) = 0$	$\Delta_1(K_4) = -3$
$\Delta_2(K_1) = -81$	$\Delta_2(K_2) = -81$	$\Delta_2(K_3) = -81$	$\Delta_2(K_4) = 27$
<b>nema odluke</b>	<b>nema ekstrema</b>	<b>nema odluke</b>	<b>maksimum</b>

Kako je  $f(K_1) = f(K_3) = 0 < f(K_4) = 13.5$ , a nama treba maksimalni tok, ne trebamo dodatno ispitivati.

Znači, za kvadar ( $a=3, b=1.5, c=1$ ) imamo maksimalni tok koji iznosi

$$f(K_4) = 13.5$$



**1011 - I2 - 5**

Dokažite:

- a) Tenzor ranga 2 može se napisati kao zbroj simetričnog i antisimetričnog tenzora.
- b) Ako je rang tenzora  $\tilde{A}$  i  $\tilde{B}$  naznačen brojem indeksa u relacija  $K^{ijkl} A_{ij} = B^{kl}$ , koja vrijedi u svim (zarotiranim) Kartezijevim sustavima, tada je  $\tilde{K}$  tenzor ranga 4.

**a)**

Kako su dokazi za kovarijantne, kontravarijantne i miješane tenzore slični, dokazat ćemo za kontravarijantni:

$$T^{ij} = \frac{1}{2}T^{ij} + \frac{1}{2}T^{ij}$$

Dodamo li i oduzmemo  $T^{ji}/2$  nećemo promijeniti tenzor

$$T^{ij} = \frac{T^{ij} + T^{ji}}{2} + \frac{T^{ij} - T^{ji}}{2}$$

Zamjena indeksa odgovara transponiranju matrice reprezentacije vektora pa ako transponiramo prvi sumand

$$\left(\frac{T^{ij} + T^{ji}}{2}\right)^{\tau} = \frac{(T^{ij})^{\tau} + (T^{ji})^{\tau}}{2} = \frac{T^{ji} + T^{ij}}{2} = \frac{T^{ij} + T^{ji}}{2}$$

dobijemo isto, što znači

$$\frac{T^{ij} + T^{ji}}{2}$$

simetrični je tenor. Transponiranjem drugog dobijemo

$$\left(\frac{T^{ij} - T^{ji}}{2}\right)^{\tau} = \frac{(T^{ij})^{\tau} - (T^{ji})^{\tau}}{2} = \frac{T^{ji} - T^{ij}}{2} = -\frac{T^{ij} - T^{ji}}{2}$$

što znači

$$\frac{T^{ij} - T^{ji}}{2}$$

antisimetrični je tenzor pa tenzor ranga 2 možemo napisati kao zbroj simetričnog i antisimetričnog tenzora.

**b)**

Dana relacija vrijedi u svim (zarotiranim) Kartezijevim sustavima pa ćemo je napisati u crtkanome

$$K'^{ijkl} A'_{ij} = B'^{kl} = a_m^k a_n^l B^{mn} = \quad // \text{ B transformiramo u necrtkani sustav}$$

$$= a_m^k a_n^l (K^{opmn} A_{op}) = \quad // \text{ Primijenimo kvocijentno pravilo}$$

$$= a_m^k a_n^l (K^{opmn} a_o^i a_p^j A'_{ij}) = \quad // \text{ A transformiramo u crtkani}$$

$$= a_o^i a_p^j a_m^k a_n^l K^{opmn} A'_{ij}$$

$$K'^{ijkl} A'_{ij} = a_o^i a_p^j a_m^k a_n^l K^{opmn} A'_{ij} \quad // \text{ Izjednačimo početak i kraj jednakosti}$$

$$(K'^{ijkl} - a_o^i a_p^j a_m^k a_n^l K^{opmn}) A'_{ij} = 0 \quad // \text{ A općenit pa je izraz u zagradi 0}$$

$$K'^{ijkl} = a_o^i a_p^j a_m^k a_n^l K^{opmn} \quad // \text{ Način transformacije tenzora 4. ranga}$$